In the claims:

Please amend the claims pending in the application as reflected in the following listing:

- 1. (Original) A space variant polarization optical element for spatially manipulating polarization-dependent geometrical phases of an incident light beam, the element comprising a substrate comprising a plurality of zones of gratings with a continuously varying orientation, the orientation denoted by $\theta(x, y)$ which is equal to half of a desired geometrical phase (DGP) modulus 2π , each grating with a local period that is smaller than the wavelength of the incident light beam.
- 2. (Original) The optical element of claim 1, wherein the orientation of the grating satisfies the equation $2\theta(x,y) = \pi r^2/\lambda f\Big|_{\text{mod}2\pi}$, where f is a desired focal length and λ is the wavelength of the incident light beam, whereby the optical element is used as a converging lens if the incident light beam exhibits right-hand circular polarization, and as a diverging lens if the incident light beam exhibits left-hand circular polarization.
- 3. (Original) The optical element of claim 1, wherein the following relation is maintained $\nabla \times \mathbf{K}_g = 0$, where $\mathbf{K}_g = K_0(x, y) [\cos(\varphi_d(x, y)/2)\hat{\mathbf{x}} + \sin(\varphi_d(x, y)/2)\hat{\mathbf{y}}]$, where \mathbf{K}_g is a grating vector, $\hat{\mathbf{x}}$ and $\hat{\mathbf{y}}$ are unit vectors in the x and y direction, $K_0 = 2\pi/\Lambda(x, y)$, where K_0 is the spatial frequency of the grating, Λ is the local period of the grating and $\varphi_d(x, y)/2$ is the space-variant direction of the vector so that it is perpendicular to the grating stripes at any given point.
- 4. (Original) The optical element of claim 1, used as diffraction grating element, wherein the following equation is maintained $\varphi_d = (2\pi/d)x|_{\text{mod}2\pi}$, where d is the period of the plurality of zones, and wherein the grating satisfies the relation
- $\phi_g(x,y) = (2d/\Lambda_0)\sin(\pi x/d)\exp(-\pi y/d)$, where Λ_0 is the local period of the grating at y=0.
- 5. (Original) The optical element of claim 1, wherein the substrate is a wafer.
- 6. (Original) The optical element of claim 5, wherein the wafer is manufactured using photolithography techniques.
- 7. (Original) The optical element of claim 6, wherein the wafer is manufactured using etching.

- 8. (Original) The optical element of claim 1, wherein the grating is in blazed form, with opposite blazed directions for incident left-hand circular polarization and for right-hand circular polarization, of the incident light beam.
- 9. (Original) The optical element of claim 1, wherein the orientation of the gratings varies linearly in a predetermined direction.
- 10. (Original) The optical element of claim 1, wherein the orientation of the grating of the zones satisfies the equation $\theta(x) = -\pi x/d|_{\text{mod}\pi}$, where $\theta(x)$ is the orientation of a grating line at a position x on an axis, and d is the period of the orientation of the grating of the zones.
- 11. (Original) The optical element of claim 1, wherein it is used as an optical switch.
- 12. (Original) The optical element of claim 1, wherein it is used as a beam-splitter.
- 13. (Original) The optical element of claim 1, used as a Lee-type binary subwavelength structure mask.
- 14. (Original) The optical element of claim 1, wherein it is used for polarimetry.
- 15. (Original) The optical element of claim 1, wherein the grating in each zone comprise of at least two regions of gratings arranged in different orientations.
- 16. (Original) The optical element of claim 1, wherein the following relation is satisfied, $\theta(x, y) = \omega(x, y) + c$, where x and y are coordinates of a specific position in an orthogonal set of axes, $\omega = \arctan(y/x)$ is the azimuthal angle, and c is a constant.
- 17. (Original) The optical element of claim 1, wherein the orientation of the grating is spiral.
- 18. (Original) The optical element of claim 1, wherein the orientation of the grating satisfies the relation $\theta(r,\omega) = l\omega/2$, where *l* is a topological charge, and r,ω indicate a specific angular position at radius r and angle ω .
- 19. (Original) The optical element of claim 18, wherein the grating satisfy the relation $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0)(r_0/r)^{l/2-1}\cos[(l/2-1)\omega]/[l/2-1] \text{ for } l \neq 2, \text{ and}$ $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0)\ln(r/r_0) \text{ for } l = 2, \text{ where } \Lambda_0 \text{ is the local period of the grating }.$
- 20. (Original) A space variant polarization optical element for spatially manipulating polarization-dependent geometrical phases of an incident light beam, the element comprising a substrate comprising a plurality of zones of gratings with discretely varying orientation, the

orientation denoted by $\theta(x, y)$ which is equal to half of a desired geometrical phase (DGP) modulus 2π , each grating with a local period that is substantially smaller than the wavelength of the incident light beam.

- 21. (Original) The optical element of claim 20, wherein the discretely varying orientation comprises rotated orientation.
- 22. (Original) The optical element of claim 21, wherein the rotated orientation varies linearly.
- 23. (Original) The optical element of claim 20, used as diffraction grating element, wherein the following equation is maintained $\varphi_d = (2\pi/d)x|_{\text{mod}2\pi}$, where d is the period of the plurality of zones, and wherein the grating satisfies the relation
- $\phi_{g}(x,y) = (2d/\Lambda_{0})\sin(\pi x/d)\exp(-\pi y/d)$, where Λ_{0} is the local period of the grating at y=0.
- 24. (Original) The optical element of claim 20, wherein the substrate is a wafer.
- 25. (Original) The optical element of claim 20, wherein the wafer is manufactured using photolithography techniques.
- 26. (Original) The optical element of claim 25, wherein the wafer is manufactured using etching.
- 27. (Original) The optical element of claim 20, wherein the orientation of the grating of the zones satisfies the equation $\theta(x) = -\pi x/d|_{\text{mod }\pi}$, where $\theta(x)$ is the orientation of a grating line at a position x on an axis, and d is the period of the orientation of the grating of the zones.
- 28. (Original) The optical element of claim 20, wherein it is used as an optical switch.
- 29. (Original) The optical element of claim 20, wherein it is used as a beam-splitter.
- 30. (Original) The optical element of claim 20, used as a Lee-type binary subwavelength structure mask.
- 31. (Original) The optical element of claim 20, wherein it is used for polarimetry.
- 32. (Original) The optical element of claim 20, wherein the grating in each zone comprise of at least two regions of gratings arranged in different orientations.
- 33. (Original) The optical element of claim 20, wherein the following relation is satisfied, $\theta(x, y) = \omega(x, y) + c$, where x and y are coordinates of a specific position in an orthogonal set of axes, $\omega = \arctan(y/x)$ is the azimuthal angle, and c is a constant.

- 34. (Original) The optical element of claim 20, wherein the orientation of the grating satisfies the relation $\theta(r,\omega) = l\omega/2$, where l is a topological charge, and r,ω indicate a specific angular position at radius r and angle ω .
- 35. (Original) The optical element of claim 34, wherein the grating satisfy the relation $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0)(r_0/r)^{l/2-1}\cos[(l/2-1)\omega]/[l/2-1] \text{ for } l \neq 2, \text{ and}$ $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0)\ln(r/r_0) \text{ for } l = 2, \text{ where } \Lambda_0 \text{ is the local period of the grating }.$
- 36. (Original) The optical element of claim 20, wherein the zones of gratings are arranged in an annular manner.
- 37. (Original) The optical element of claim 20, wherein the zones of gratings are arranged in a coaxial manner.
- 38. (Original) A method for spatially manipulating polarization-dependent geometrical phases of an incident light beam, the method comprising: providing a substrate comprising a plurality of zones of gratings, with a continuously varying orientation, the orientation denoted by $\theta(x, y)$ which is equal to half of a desired geometrical phase (DGP) modulus 2π , each grating having a local period that is smaller than the wavelength of the incident light beam irradiating the incident light beam onto the substrate.
- 39. (Original) The method of claim 38, wherein the orientation of the grating satisfies the equation $2\theta(x,y) = \pi r^2/\lambda f\Big|_{\text{mod}2\pi}$, where f is a desired focal length and λ is the wavelength of the incident light beam, whereby the optical element is used as a converging lens if the incident light beam exhibits right-hand circular polarization, and as a diverging lens if the incident light beam exhibits left-hand circular polarization.
- 40. (Original) The method of claim 38, wherein the following relation is maintained $\nabla \times \mathbf{K}_g = 0$, where $\mathbf{K}_g = K_0(x, y) [\cos(\varphi_d(x, y)/2)\hat{\mathbf{x}} + \sin(\varphi_d(x, y)/2)\hat{\mathbf{y}}]$, where K_g is a grating vector, $\hat{\mathbf{x}}$ and $\hat{\mathbf{y}}$ are unit vectors in the x and y direction, $K_0 = 2\pi/\Lambda(x, y)$, where K_0 is the spatial frequency of the grating, Λ is the local period of the grating and $\varphi_d(x, y)/2$ is the space-variant direction of the vector so that it is perpendicular to the grating stripes at any given point.

- 41. (Original) The method of claim 38, used as diffraction grating element, wherein the following equation is maintained $\varphi_d = (2\pi/d)x\big|_{\text{mod} 2\pi}$, where d is the period of the plurality of zones, and wherein the grating satisfies the relation $\phi_g(x,y) = (2d/\Lambda_0)\sin(\pi x/d)\exp(-\pi y/d)$, where Λ_0 is the local period of the grating at y=0.
- 42. (Original) The method of claim 38, wherein the grating is in blazed form, with opposite blazed directions for incident left-hand circular polarization and for right-hand circular polarization, of the incident light beam.
- 43. (Original) The method of claim 38, wherein the orientation of the gratings varies linearly in a predetermined direction.
- 44. (Original) The method of claim 38, wherein the orientation of the grating of the zones satisfies the equation $\theta(x) = -\pi x/d|_{\text{mod }\pi}$, where $\theta(x)$ is the orientation of a grating line at a position x on an axis, and d is the period of the orientation of the grating of the zones.
- 45. (Original) The method of claim 38, wherein it is used for optical switching.
- 46. (Original) The method of claim 38, wherein it is used for beam-splitting.
- 47. (Original) The method of claim 38, wherein it is used for polarimetry.
- 48. (Original) The method of claim 38, wherein the grating in each zone comprise of at least two regions of gratings arranged in different orientations.
- 49. (Original) The method of claim 38, wherein the following relation is satisfied, $\theta(x, y) = \omega(x, y) + c$, where x and y are coordinates of a specific position in an orthogonal set of axes, $\omega = \arctan(y/x)$ is the azimuthal angle, and c is a constant.
- 50. (Original) The method of claim 38, wherein the orientation of the grating is spiral.
- 51. (Original) The method of claim 38, wherein the orientation of the grating satisfies the relation $\theta(r,\omega) = l\omega/2$, where l is a topological charge, and r,ω indicate a specific angular position at radius r and angle ω .
- 52. (Original) The method of claim 51, wherein the grating satisfy the relation $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0)(r_0/r)^{l/2-1}\cos[(l/2-1)\omega]/[l/2-1] \text{ for } l \neq 2, \text{ and}$ $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0)\ln(r/r_0) \text{ for } l = 2, \text{ where } \Lambda_0 \text{ is the local period of the grating }.$

- 53. (Original) A method for spatially manipulating polarization-dependent geometrical phases of an incident light beam, the method comprising: providing a substrate comprising a plurality of zones of gratings with discretely varying orientation, the orientation denoted by $\theta(x, y)$ that is equal to half of a desired geometrical phase (DGP) modulus 2π , each grating with a local period that is substantially smaller than the wavelength of the incident light beam; irradiating the light beam on the substrate.
- 54. (Original) The method of claim 53, wherein the discretely varying orientation comprises rotated orientation.
- 55. (Original) The method of claim 54, wherein the rotated orientation varies linearly.
- 56. (Original) The method of claim 54, used as diffraction grating element, wherein the following equation is maintained $\varphi_d = (2\pi/d)x\big|_{\text{mod }2\pi}$, where d is the period of the plurality of zones, and wherein the grating satisfies the relation $\phi_g(x,y) = (2d/\Lambda_0)\sin(\pi x/d)\exp(-\pi y/d)$, where Λ_0 is the subwavelength period at y=0.
- 57. (Original) The method of claim 54, wherein the orientation of the grating of the zones satisfies the equation $\theta(x) = -\pi x/d|_{\text{mod }\pi}$, where $\theta(x)$ is the orientation of a grating line at a position x on an axis, and d is the period of the orientation of the grating of the zones.
- 58. (Original) The method of claim 53, wherein it is used for optical switching.
- 59. (Original) The method of claim 53, wherein it is used for beam-splitting.
- 60. (Original) The method of claim 53, wherein it is used for polarimetry.
- 61. (Original) The method of claim 53, wherein the grating in each zone comprise of at least two regions of gratings arranged in different orientations.
- 62. (Original) The method of claim 53, wherein the following relation is satisfied, $\theta(x,y) = \omega(x,y) + c$, where x and y are coordinates of a specific position in an orthogonal set of axes, $\omega = \arctan(y/x)$ is the azimuthal angle, and c is a constant.
- 63. (Original) The method of claim 53, wherein the orientation of the grating satisfies the relation $\theta(r,\omega) = l\omega/2$, where *l* is a topological charge, and r,ω indicate a specific angular position at radius r and angle ω .

- 64. (Original) The method of claim 63, wherein the grating satisfy the relation $\phi_g(r,\omega) = (2\pi r_0 / \Lambda_0)(r_0 / r)^{l/2-1} \cos[(l/2-1)\omega] / [l/2-1] \text{ for } l \neq 2, \text{ and}$
- $\phi_g(r,\omega) = (2\pi r_0/\Lambda_0) \ln(r/r_0)$ for l=2, where Λ_0 is the local period of the grating.
- 65. (Original) The method of claim 53, wherein the zones of gratings are arranged in an annular manner.
- 66. (Original) The method of claim 53, wherein the zones of gratings are arranged in a coaxial manner.
- 67-68. (Cancelled)